



# CHARACTERIZATION AND PROCESS DEVELOPMENT OF CYANATE ESTER RESIN COMPOSITES

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# OBJECTIVES

- Investigate the effects of the cure cycle and process environment on cyanate ester resin and composite properties
- Develop a high-strength hoop-wound composite by the wet-filament winding method
  - Toray T1000G carbon fiber
  - YLA RS-14A (or RS-14) cyanate ester resin

# CYANATE ESTER RESINS

Cyanate esters are a family of monomers and prepolymers which contain reactive ring-forming cyanate ( $-O-C\equiv N$ ) functional groups

- Conversion, or curing, occurs via cyclotrimerization to form three-dimensional triazine ring connecting units
- Additive reaction
- Exothermic
- Thermoset polycyanurate plastics

# ADVANTAGES OF CYANATE ESTER RESINS

- Low outgassing
- Low moisture absorption
- High thermal stability
- Radiation resistant
- Tough/resistant to microcracking caused by thermal cycling
- Low dielectric constant and low dissipation factors
- “Zero” net volume change with cure
- Processing flexibility
  - Prepreg lamination
  - Wet-filament winding
  - Resin transfer molding

# CYANATE ESTER RESIN

- YLA RS-14A (or RS-14) resin
  - RS-14A and RS-14 resins are identical with the exception that the RS-14 resin contains minute quantities of zirconate coupling agent.
  - RS-14 product discontinued during course of this study and replaced with the RS-14A formulation.
- Low viscosity
  - 0.2 to 0.1 Pa•s between 70° to 85°C
  - Excellent wet-winding resin

# PROCESS VARIABLES

- Time-temperature profile (cure cycle)
- Thermal cycling
- Resin exposure to humidity during processing
- Resin exposure to air during cure

# CURE CYCLE VARIABLES

- Precure temperature
  - 138°C (~280°F)
  - 193°C (~380°F)
  - No precure step (ramp directly to postcure temperature)
- Postcure temperature
  - 250°C (~480°F)
  - 265°C (~510°F)
- Multiple precure and/or postcure cycles
  - Pertinent to fabrication of “thick” composite cylinders that are wound and cured in increments (“stages”)

# DSC ANALYSES

DSC analyses were conducted to determine the effects of ramp rate, precure and postcure temperature on the resin's ultimate  $T_g$  and cure profile

- Cure Cycle
  - 138°C (~280°F) versus 193°C (~380°F) precure step
  - No precure step (ramp directly to postcure temperature)
  - 250°C (~480°F) versus 265°C (~510°F) postcure step
- Ramp rate
  - 1°, 2°, and 4°C/min ramp rate to temperature
- Dwell times
  - 3 h precure
  - 4 h postcure



## DSC data for cyanate ester resin

Resin	135°C		190°C		250°C		265°C		T <sub>g</sub> °C	Enthalpy J/g
	Ramp °C/min	Hold h	Ramp °C/min	Hold h	Ramp °C/min	Hold h	Ramp °C/min	Hold h		
RS-14							1	4	253	-774
							2	4	256	-624
							4	4	255	-519
							4	4	253	-539
					1	4			256	-616
					2	4			254	-536
					2	4			256	-538
					4	4			255	-472
	1	3					1	4	253	-
	1	3					1	4	255	-
	4	3					1	4	254	-
			1	3			1	4	254	-
			4	3			1	4	256	-
			4	3			1	4	256	-
RS-14A							2	4	270	-570
							2	4	270	-598

# DSC RESULTS

- $T_g$  the same for all cure cycles investigated
  - RS-14: 253° to 256°C
  - RS-14A: 270°C
- $T_g$  the same for samples postcured at 250°C or 265°C
  - long (4 h) dwell time enables cyclotrimerization to proceed to same degree of conversion for both postcure temperatures

# RESIN PANELS

Resin panels were fabricated and tested to determine effects of cure cycle and process environment on cyanate ester resin's properties

- Cure cycle
  - 138°C versus 193°C precure step
  - No precure step (ramp directly to postcure temperature)
  - 250°C versus 265°C postcure step
- Process environment
  - air
  - inert (nitrogen)
- Thermal cycling to precure or postcure temperature
  - 3 to 4 cycles

# RESIN PANEL EVALUATION

- Tensile properties
  - strength
  - modulus
  - elongation
- $T_g$ 
  - DMA
  - Line-fit intercept method using storage modulus ( $G'$ ) curve
- Density

# RESIN PANEL RESULTS

Comparable RS-14A and RS-14 resin properties were obtained for all of the process cycles conducted a single time (non-thermally cycled) and in a nitrogen environment

- Tensile properties
  - 82 to 90 MPa strength
  - 2.6 to 3.0 GPa modulus
  - 4.1 to 5.5% elongation
- $T_g$ 
  - RS-14  $T_g$ : 242° to 255°C
  - RS-14A  $T_g$ : 262° to 263°C  $T_g$
- Density
  - ~1.20 g/cm<sup>3</sup>

# AIR VS INERT (N<sub>2</sub>) CURE

- Panels exposed to air at elevated temperatures during cure had significantly **lower** tensile strengths and elongations than panels processed in nitrogen
  - Dark brown-black layer at panel surface
  - Dark layer hypothesized to act as flaw to promote premature tensile failure in specimens

## AIR VS INERT (N<sub>2</sub>) CURE (cont'd)

- Properties of panel thermally cycled to 193°C precure temperature in air similarly degraded even though later postcured in nitrogen
  - Slight darkening of panel surface with each thermal cycle
  - Reduced tensile strength and elongation
  - 10° to 20°C reduction in T<sub>g</sub>
- Properties of panel thermally cycled to 138°C precure temperature in air unaffected
  - No surface reaction (coloration) evident

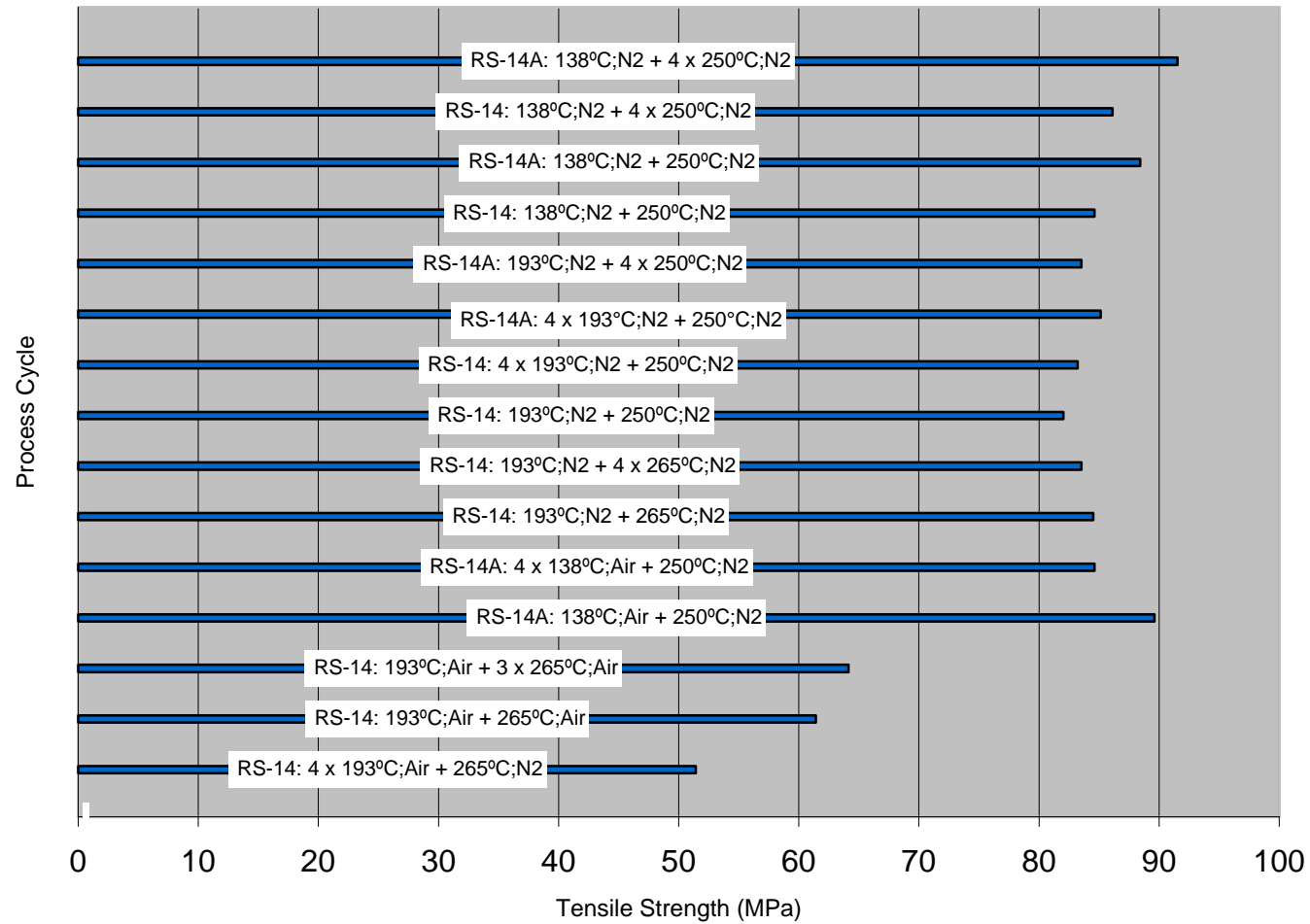
# THERMAL CYCLING

No significant change in resin properties with multiple precure and postcure cycles for panels that were maintained in a nitrogen environment

- Additional postcure cycles to either 250° or 265°C did not appreciably change resin  $T_g$
- Multiple thermal cycles to 265°C postcure temperature in nitrogen significantly darkened resin with each cycle
  - Coloration visible throughout entire thickness of resin panel



RS-14 and RS-14A Resin  
Tensile Strength Versus Process Cycle



# HUMIDITY EXPOSURE

A study was conducted to characterize the effects of humidity (moisture) exposure during processing on the cured cyanate ester resin properties

- Simulate wet-filament winding environments
- Establish “thresholds” or limits at which the cyanate ester resin’s properties are compromised by moisture exposure

# RESIN PRECONDITIONING

- Uncured resin samples exposed to a range of humidity levels in an environmental chamber
  - 80°C
  - 2, 4, and 8 h exposures
  - Continuous stirring
- Resin evaluation
  - Water content (Karl-Fischer titration)
  - $T_g$  (DSC)
  - Cured resin properties
    - Tensile strength, modulus and elongation
    - $T_g$  (DMA)

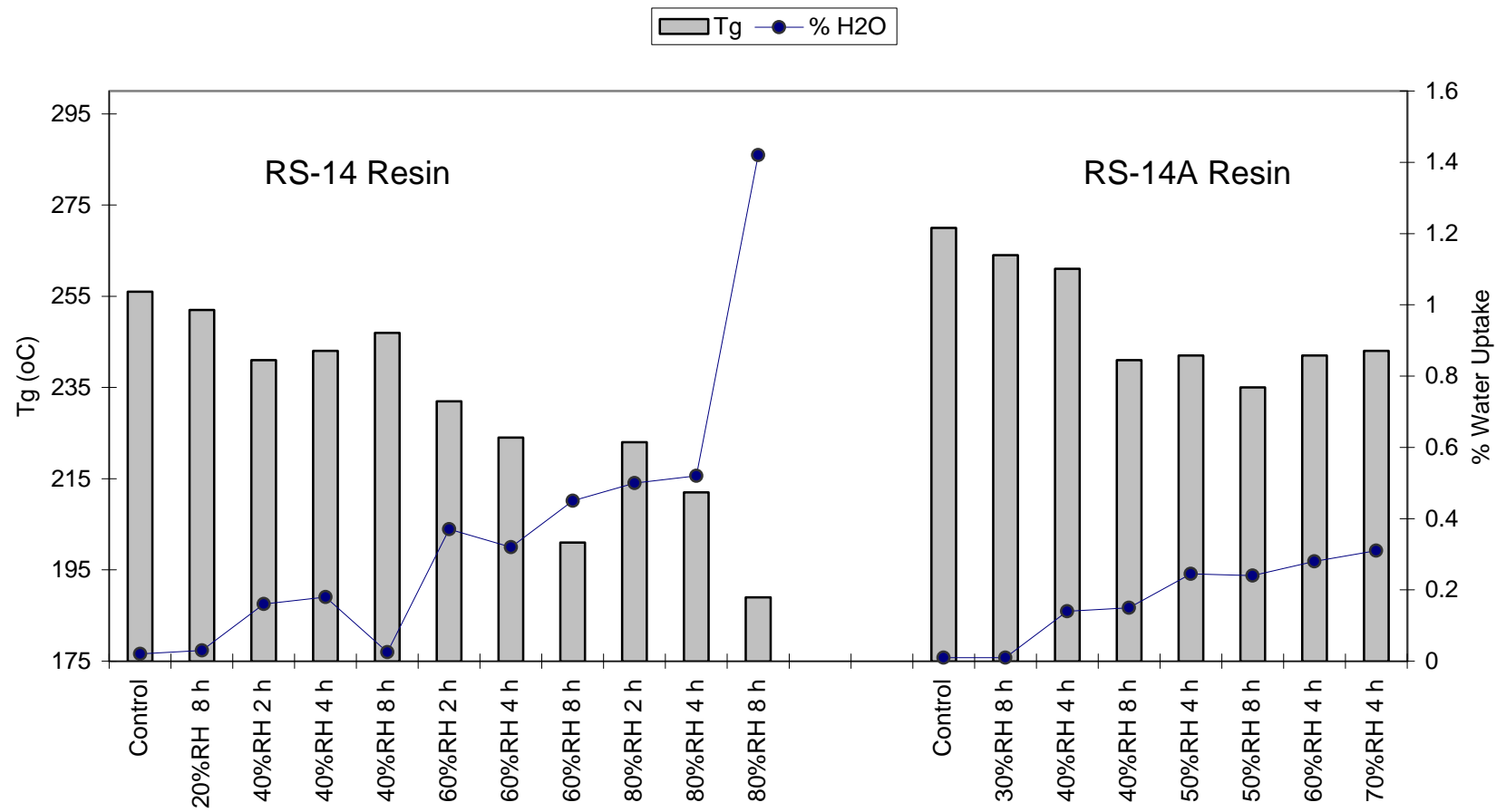
### Effects of humidity exposure (80°C) on cyanate ester resin properties

Resin	Exposure		Karl-Fischer Water %	DSC T <sub>g</sub> °C	Strength MPa	Tensile		DMA T <sub>g</sub> °C
	RH %	Time h				Modulus GPa	Elongation %	
RS-14	Control		0.02	256	89.8	2.7	5.8	252
	20	8	0.03	252	85.2	2.8	4.8	252
	40	2	0.16	241	91.4	2.7	5.9	243
	40	4	0.21/0.15	243	89.6	2.7	5.3	237
	40	8	0.03/0.02	247	90.4	2.8	5.5	248
	60	2	0.37	232	87.3	2.8	4.8	233
	60	4	0.38/0.26	224	83.9	2.8	4.4	227
	60	8	0.45	201	(Extensive bubbles and voids in panel)			206
	80	2	0.50	223	87.0	2.7	4.9	236
	80	4	0.52	212	88.7	2.8	5.0	231
	80	8	1.42	189	(Extensive bubbles and voids in panel)			199
RS-14A	Control		0.01	270	88.4	2.6	5.5	262
	30	8	0.01	264	88.5	2.7	5.2	259
	40	4	0.14	261	86.4	2.7	5.1	258
	40	8	0.15	241	89.5	2.8	5.2	247
	50	4	0.21/0.28	242	91.1	2.7	5.3	251
	50	8	0.16/0.31	235	88.3	2.8	5.1	238
	60	4	0.28	242	93.2	2.8	5.1	240
	70	4	0.31	243	(Extensive bubbles and cracks in panel)			238

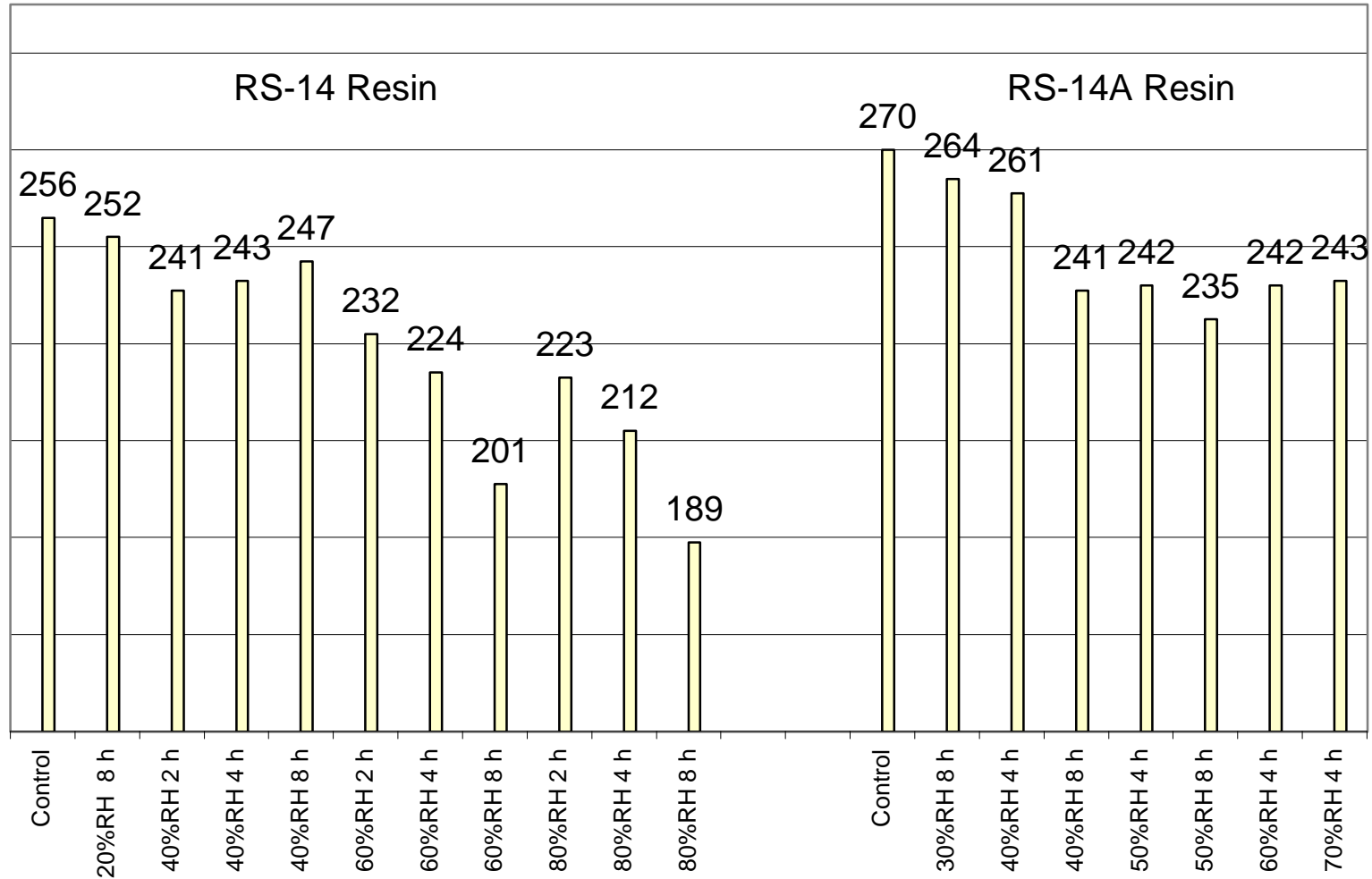
# HUMIDITY EFFECTS ON RESIN

- Significant  $T_g$  reductions with increasing humidity exposure and water uptake
  - Slight  $T_g$  reductions after 8 h at 30% RH
  - Greatest  $T_g$  reductions with exposures greater than 40% RH
  - Water content increases from 0.01 to 0.02% (as-received) level to above 0.1% after 2 h at 40% RH
- Large bubbles in panels cast from resin preconditioned to 60% and 80% RH
- Tensile properties unaffected by high humidity exposures!

RS-14 and RS-14A Resin  
Glass Transition Temperature (°C) Versus Humidity Exposure



**RS-14 and RS-14A Resin**  
**Glass Transition Temperature (°C) Versus Humidity Exposure**



# CARBAMATE FORMATION

The degradation of thermal properties is attributed to the reaction of the cyanate function with water (hydrolysis) leading to the production of a carbamate species

- Carbamates decompose above 190°C, yielding an amine and CO<sub>2</sub>
- CO<sub>2</sub> evolution can lead to bubbles and voids in resin and composite samples
- Triazine ring formation process interrupted
  - Reduced cyanate functionality due to carbamate formation
  - Amine resulting from carbamate decomposition can react with another cyanate group, leading to a linear species with reduced properties (lower T<sub>g</sub>)



# COMPOSITE PROCESS TRIALS

Composite process trials were conducted to investigate the effects of cure cycle and process environment on composite mechanical properties

- Cure cycles (extension of resin process trials)
  - 138°C and 193°C precure step
  - No precure step (ramp directly to postcure temperature)
  - 260° or 265°C postcure step
  - 3 h precure & 4 h postcure
- Air versus inert atmosphere cure
- Thermal cycling (on mandrel) during manufacture
  - 3 to 4 cycles
  - Pertinent to fabrication of “thick” cylinders that are wound and cured in stages

# COMPOSITE CYLINDERS

- All-hoop wet-filament wound composite
- ~610 mm ID x 3.18 mm wall thickness
- T1000G carbon fiber
  - Single lot
  - 6,577 MPa (954 ksi) fiber strength
  - Lot average measured by ORNL
- YLA RS-14A or RS-14 resin

# CYLINDER EVALUATION

- Ring (hoop) tensile strength and modulus
  - “Split-D” method based on ASTM D2290
  - Extensometer-measured “D” separation (modulus)
- Interlaminar shear strength
  - ASTM D2344
- Transverse flexure strength
  - ASTM D790
  - OD surface in tension
- Composition
  - Calculated from composite density (ASTM D792) and weight percent resin and fiber contents (nitric acid digestion)

## Composite process trial results

Process Environment	Air				Inert (N <sub>2</sub> )						
Precure	193°C	193°C	138°C	4 x 138°C	138°C	4 x 138°C	193°C	4 x 193°C	193°C	None	None
Postcure	265°C	3 x 265°C	260°C	260°C	260°C	260°C	260°C	260°C	4 x 260°C	260°C	4 x 260°C
Resin	RS-14	RS-14	RS-14	RS-14	RS-14A	RS-14A	RS-14A	RS-14A	RS-14A	RS-14A	RS-14A
<b>Ring Tensile</b>											
Strength (MPa)	4352.6	3911.4	4269.9	4560.8	4421.6	4409.2	4376.1	4640.8	4301.6	4524.3	4449.2
Modulus (GPa)	225.4	223.3	225.5	225.4	229.6	226.8	225.4	227.5	227.5	228.9	228.9
<b>SBS Strength (MPa)</b>	65.2	67.2	66.5	55.6	59.9	65.0	67.2	65.7	65.7	66.8	69.1
<b>Transverse Flexure Strength (MPa)</b>	97.1	86.9	74.4	68.9	71.6	71.4	80.3	74.0	81.9	78.9	73.1
<b>Composition</b>											
Density (g/cm <sup>3</sup> )	1.6607	1.6667	1.6575	1.6569	1.6611	1.6646	1.6648	1.6658	1.6648	1.6663	1.6663
Volume % Fiber	78.4	79.6	78.4	78.3	78.6	78.7	79.2	79.0	79.2	79.5	79.5
Volume % Resin	21.5	20.1	21.1	21.3	21.2	21.4	20.6	21.0	20.6	20.3	20.3
Volume % Voids	0.1	0.3	0.5	0.4	0.2	-0.1	0.2	0.0	0.2	0.2	0.2

### Notes:

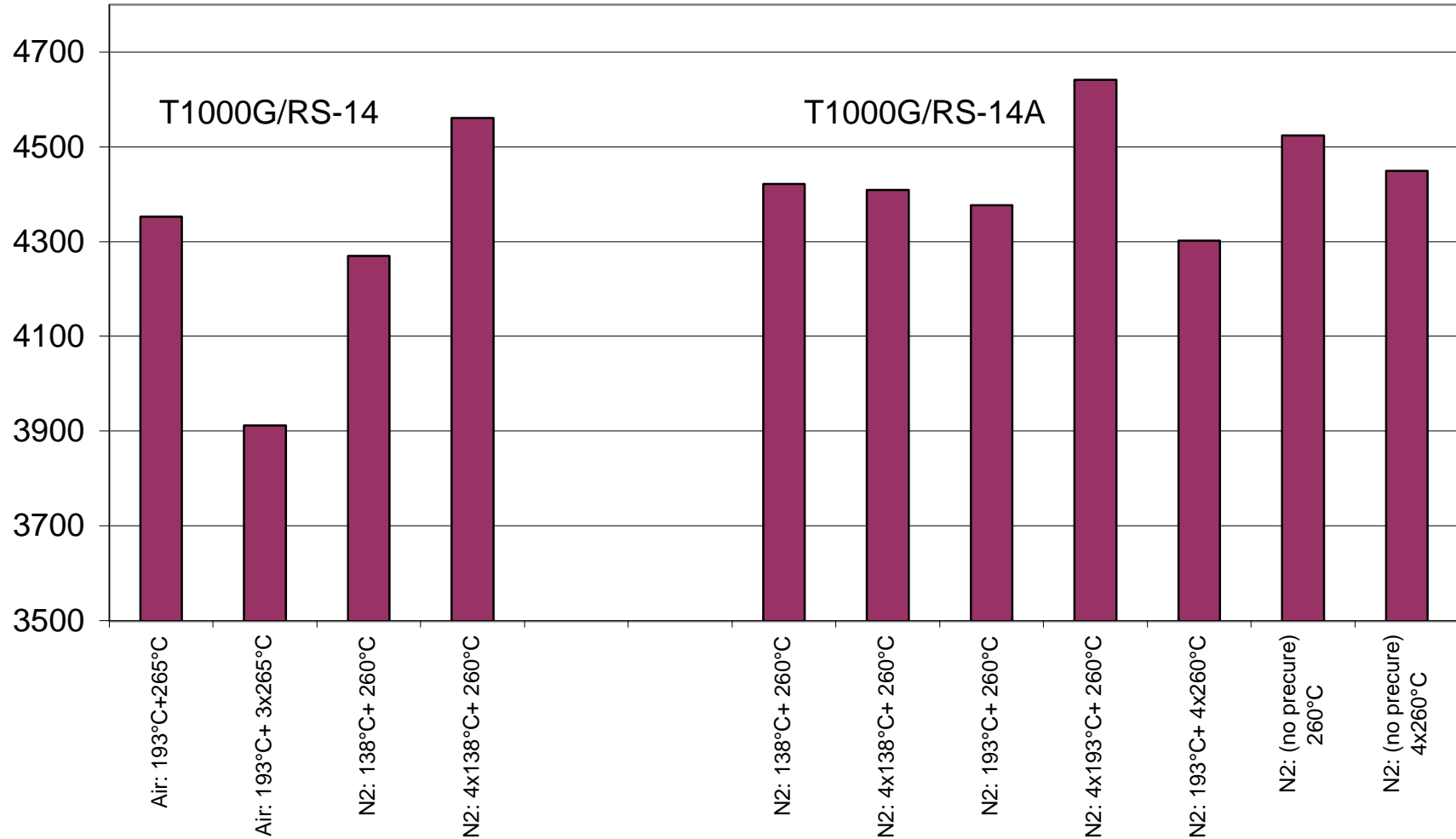
- (1) Times at process temperature are 3 h for the precure segment and 4 h for the postcure segment.
- (2) Cylinders that received additional precure or postcure cycles are indicated by the "number of cycles x" designation.

# THERMAL CYCLING IN AIR

Cylinder cycled to postcure temperature in air had significantly lower ring tensile strength than cylinders cycled in an inert atmosphere

- Black discoloration of OD surface resin for air-processed cylinders (versus amber-brown tint of N<sub>2</sub>- processed cylinders)
- Ring tensile strength reduction attributed to reduction in cyanate ester resin tensile properties as a result of reaction with air and/or moisture at elevated temperature
- Comparable to results from resin panel study
- Increase in transverse flexural strength

# T1000G/RS-14 or RS-14A Composite Ring Tensile Strength (MPa) Versus Process Cycle



# PROCESS TRIAL RESULTS

There is a broad process envelope for processing composites that are wet-filament wound with RS-14 and RS-14A resin

- Comparable composite properties achieved for all process cycles conducted in an inert atmosphere
- No affect on composite properties from additional precure and postcure cycles when conducted in an inert atmosphere

# COMPOSITE COMPOSITION

The cylinders were wound reproducibly and have nominally the same compositions

- Density:  $\sim 1.66 \text{ g/cm}^3$
- Fiber content: 78.3 to 79.6 vol.%
- Voids:  $< 0.5 \text{ vol.}\%$



# COMPOSITE PROPERTIES

- Ring tensile strength
  - 4270 to 4641 MPa
  - Individual ring strengths above 4826 MPa (*700 ksi*)
  - Highest fiber strength translations: ~89%
- Ring tensile modulus
  - 223 to 230 GPa

# COMPOSITE PROPERTIES (cont'd)

- Interlaminar shear strength
  - 56 to 69 MPa
- Transverse flexure strength
  - 69 to 82 MPa

# ELEVATED TEMPERATURE PROPERTIES

Test Temperature Stat 17 Result	20°C		60°C		135°C	
	Average	B-Basis*	Average	B-Basis*	Average	B-Basis*
<b>Ring Tensile</b> Strength (MPa)	-	-	4508.4 (2.2)	4232.7	4242.3 (1.4)	4051.3
Modulus (GPa)	-	-	224.1	-	224.1	-
<b>SBS Strength</b> (MPa)	57.4 (4.7)	51.0	56.7 (4.3)	49.7	50.9 (4.4)	44.7
<b>Transverse Flex.</b> <b>Strength (MPa)</b>	75.2 (5.3)	62.9	69.4 (5.1)	60.4	65.5 (6.0)	55.2

\* B-Basis value is from two-parameter Weibull calculation

( ) number in parenthesis is percent coefficient of variation

# SUMMARY

Process trials were conducted to determine the effects of the cure cycle and environment on cyanate ester resin and composite properties

- YLA RS-14A resin has a broad process envelope provided that the cure is conducted in an inert atmosphere
- Exposure to air at elevated temperatures produces a black reaction layer that reduces resin tensile strength and elongation
- Exposure to moisture prior to cure reduces the resin's glass transition temperature

## SUMMARY (cont'd)

High fiber fraction (78-80 vol.%) T1000G/RS-14A composite cylinders were wet-filament wound and cured in an inert ( $N_2$ ) atmosphere

- Excellent ring tensile strengths
  - Highest average cylinder strength: 4641 MPa (673 ksi)
  - Highest individual ring strengths: 4826 MPa (700 ksi)
- Good transverse properties for such high fiber fraction composites
- Excellent strength retention at elevated temperatures

# APPLICATIONS

Potential applications for these materials include flywheel energy storage systems for space and satellite structures